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PCB mass budget in a perialpine lake undergoing natural decontamination in a context of global change.

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6 **1.** Introduction:

Lake PCB (polychlorobiphenyl) contamination has been extensively studied worldwide, and the mass 7 8 budget was evaluated to highlight the main fluxes driving the PCB dynamics in lakes. Many studies 9 have investigated the American Great Lakes, which have been undergoing important PCB 10 contamination since the 1970s. The PCB mass budget for Lake Michigan shows that the most important flux responsible for decontamination was volatilization followed by sedimentation^{1,2}. The 11 12 same pattern was observed in 1994 for Lake Superior³. In Europe, small rural Lake Cumbria (England) 13 showed important PCB contamination resulting from surface water runoff. The mass budget 14 indicated that a large part of the decontamination was due to outflow and volatilization⁴. The same 15 conclusion was drawn for several high-altitude lakes⁵⁻⁸. PCB mass budgets are based on a compilation of the measured and estimated fluxes to which uncertainties are inherently associated. 16 17 Indeed, several fluxes (i.e., sediment resuspension and molecular diffusion at the air/water and sediment/water interfaces) are often modeled considering important uncertainties^{9,10}. These 18 19 uncertainties are related to the approximations of PCB quantification methods, analysis and 20 partitioning constants (i.e., Henry's law constant and the octanol-water partition coefficient). The 21 impacts of these uncertainties on the calculated fluxes should be identified and considered to build 22 accurate PCB mass budgets.

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24 PCB mass budgets are lake-dependent given that a lake's trophic and physical or chemical 25 characteristics influence its contaminant flux. Although the American Great Lakes have been 26 extensively studied and a few studies have focused on the particular case of high-altitude mountain 27 lakes, information concerning medium-sized perialpine lakes remains scarce. A few studies have investigated Lake Geneva (France/Switzerland) ^{11–13} and Lake Maggiore, as well as Lake Lugano in 28 29 Italy^{14,15}, but PCB mass budgets were not obtained. These perialpine lakes are often used as 30 resources for many activities (fishing, leisure sports, drinking water supply). In this context, it is of 31 critical importance to identify the main fluxes driving PCB dynamics in such lakes. Lake Bourget 32 (France) has similar physical and chemical characteristics to many other perialpine lakes 33 contaminated with PCBs in Europe but greatly differs from the American Great Lakes. With a 34 catchment area/lake surface area ratio of 13, a surface area/volume ratio of 12.3 and a residence 35 time of 11 years, Lake Bourget is a medium-sized (44.5 km²) perialpine lake. It is currently considered meso-oligotrophic¹⁶ (i.e., chlorophyll α concentration = 3.3 μ g·L⁻¹, total phosphorus concentration = 36 37 10 μ g.L⁻¹ and total organic carbon concentration = 1.7 mg·L⁻¹). However, lake Bourget remains heavily 38 contaminated with PCBs, and the water still exceeds the US-EPA recommended maximum 39 concentration of 170 pg·L⁻¹ for the sum of the 7 indicator PCBs (Σ 7PCB_i) for the protection of aquatic 40 wildlife.

To fill the knowledge gap regarding PCB dynamics in perialpine lakes, this study aimed to (i) establish a PCB mass budget to identify the main fluxes involved in the decontamination process and (ii) identify and accurately quantify the uncertainties associated with both measured and modeled PCBfluxes in Lake Bourget for the period of 2013-2017.

45 Our hypothesis was that volatilization and sediment burial were the main fluxes ruling the PCB 46 decontamination process in Lake Bourget. Both flux intensities are susceptible to environmental 47 factors. Indeed, as in many other perialpine lakes^{17–19}, Lake Bourget underwent a period of 48 eutrophication and is currently facing reoligotrophication. Consequently, the diminution of primary 49 production could impact the sedimentation flux of PCBs in Lake Bourget through the modification of the process of "biological pumping"^{20,21}. Therefore, the oligotrophication of the lake could reduce the 50 intensity of the flux of PCBs escaping the water column through settling and sediment burial. Alpine 51 52 regions could be particularly affected by climate change with an exacerbated increase in temperature expected compared to the moderate increase in the northern hemisphere²². Hence, relatively small 53 54 water bodies, such as perialpine lakes, could specifically experience increased water temperatures, as is already the case in Lake Bourget¹⁶. This phenomenon will be amplified in the near future with 55 perialpine lakes first affected by climate change. Since the volatilization flux of PCBs is dependent on 56 57 the water temperature, an increase in the water temperature could have an impact on the intensity 58 of the volatilization flux. Therefore, in regards to the singular situation of perialpine lakes, this study 59 considered (i) the impact of oligotrophication on the intensity of the settling and burial fluxes of PCBs 60 and (ii) the impact of an increase in water temperature on the intensity of the volatilization flux of 61 PCBs.

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2. Materials and methods

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68 **<u>2.1 Study site:</u>**

69 Lake Bourget is the largest natural lake in France, with a surface area of 44 km², a length of 18 km, a 70 width between 1.6 km and 3.5 km and a mean depth of 85 m (maximum: 145 m) (Fig. S1). Its main 71 PCB source is the Tillet River running through the city of Aix les Bains. Lake Bourget was 72 contaminated from 1930 to 1987 by an electrical transformer factory using Pyralène® (French 73 equivalent for Aroclor[®]). Ever since, the PCBs contained in sediment have been slowly released into 74 the lake and have spread throughout the whole water body. The PCB concentration could increase 75 substantially to 250 ng·L⁻¹ during rain events, with up to 1500 g·yr⁻¹ reaching the lake in that period²³. 76 Remediation measures have resulted in a decline in PCB input, but contamination still remains 77 elevated today. The Terre-nue Canal and the Leysse River run through urbanized and industrialized 78 areas and have been considered potential sources of PCBs for the lake (Fig. S1). As a direct 79 consequence of climate change, an elevation of the water temperature in Lake Bourget has been highlighted since the first records. The average water temperature at 2 m depth was 13.0°C in 1984 80 and rose constantly to 15.5°C in 2017¹⁶. Following a period of eutrophication (1950-1990), Lake 81 82 Bourget is currently on the way to oligotrophication (characterized by an increasing transparency: 3 m in 1981 and 6 m in 2017)¹⁶ 83

84 **2.2 Sampling**

85 2.2.1 Water sampling

Water from Lake Bourget was regularly sampled 5 times between May 2013 and March 2016 at an 86 87 average depth of 5 m in the middle of the lake (point B, Fig. S3). Each time, 30 L was pumped and 88 stored for 2 h at room temperature in a steel barrel until processing. Water from the Tillet River was 89 sampled with a surface water automatic sampler (Portable sampler ISCO 3700, Ijinus®) for two and 90 five weeks (in March-April 2014 and in October-November 2014, respectively) and enabled 91 continuous suspended particulate matter (SPM) concentration determination for rainy (n = 4) and 92 dry (n = 5) periods. A sediment trap was deployed alongside the automatic sampler to collect 93 sufficient amounts of settling particles for integrative PCB concentration measurements. To ensure 94 an exhaustive budget of PCB inputs through the Tillet River, three measurements of dissolved PCBs at 95 the outlet were performed in 2017. A total of 60 L of water was pumped through precleaned glass 96 fiber filters (GFF) (porosity 0.7 µm, Whatman®) followed by precleaned polyethylene foam plugs 97 (diameter = 20 mm, L = 100 mm, Ecomesure®) for the adsorption and determination of dissolved 98 PCBs. Water PCB concentrations from the Terre-Nue River and Leysse River were determined in 2014 and 2015 by the "Agence de l'eau RMC"²⁴. Water samples from Lake Bourget were brought back to 99 the laboratory and immediately pumped through precleaned (kiln-fired 2 h at 525°C) GFF and C18 100 101 (Empore[®]) filters for the retention of particulate PCBs and dissolved PCBs, respectively. Every sample 102 was wrapped in aluminum foil and stored at -16°C before analysis.

103 2.2.2 Settling particles and sediment sampling

To evaluate the PCB settling rate, three experimental setups were performed from July 2016 to July 2017. An automated sediment trap (TECHNICAP® PPS6) was set at a depth of 40 m, 200 meters from the coast (see SI). Two additional sediment traps were set up at 20 m depth, one at the same site as the automated trap and the other at the south portion of the lake (GPS coordinates: 45.656°, 5.886'). They both operated in July 2016 and in October 2016, each time for an integrative period of one month. All settling particle samples (n = 6) were stored in clean glass bottles at -16°C before analysis.

Nine sediment cores were obtained using a gravity corer (UWITEC[®]) at five locations along a northsouth transect in the lake (n = 4 in May 2013 and n = 5 in May 2015) (Fig. S3 in SI). The first centimeter of the core was collected and analyzed to determine the PCB concentration, as it represented the sedimentation of the last 2.5 years because the sedimentation rate of 0.37 cm·yr⁻¹ in Lake Bourget is considered constant²⁵. The PCB concentrations determined for these five locations were used for resuspension, sediment/water diffusion and sediment burial calculations.

116 2.2.3 Air sampling

The atmospheric bulk deposition flux was measured on the bank of Lake Bourget (GPS coordinates: 117 45.693°, 5.890') positioned under the influence of the prevailing winds. Sampling was performed 118 119 using a lab-designed stainless steel Owen gauge (surface = 0.5 m^2) equipped with a precleaned 120 polyurethane foam (PUF) plug (diameter = 20 mm, L = 100 mm, Ecomesure[®]). Sixteen samples were collected, which enabled a follow-up period of 4 years from 2013 to 2016. The sampling of gaseous 121 PCBs was performed with a precleaned PUF disk (Ø= 140 mm, H = 13 mm, Ecomesure[®]) housed in 122 protective chambers as described by Harner et al.²⁶ and deployed alongside the Owen gauge. After 123 exposure, all PUFs were retrieved, wrapped in aluminum foil and stored at -16°C before analysis. 124 125 Samples (n = 9) were collected by continuous follow up for a period of 3 years (2014 – 2016).

126 2.2.4 Fish sampling

Fish sampling was performed by professional fishermen year-round from 2013 to 2017 and was concerned with the two most emblematic fishes of Lake Bourget: the arctic char (n = 138) and whitefish (n = 110) used for human consumption²⁷. Due to their high lipid content, these species are susceptible to the bioaccumulation of large amounts of PCBs. Therefore, intensive fishing of these two species could represent a nonnegligible loss of PCBs from Lake Bourget.

132 **2.3 Chemicals**

Heptane, acetone, dichloromethane and methanol were of HPLC quality and purchased from Carlo
Erba[®]. Anhydrous sodium sulfate was purchased from Fisher Chemical[®] (analytical reagent grade).
Silica gel 60 (70-230 mesh) for column chromatography was purchased from Merck[®]. Copper was
activated with 10 mL of 1 N sulfuric acid (Chimie Plus[®]) and then rinsed three times with Milli-Q[®]
water to a neutral pH followed by rinses with acetone for water removal. A standard mixture of
indicator PCB congeners (28, 52, 101, 118, 138, 153, 180) at 10 µg·mL⁻¹ in iso-octane and the internal
standard PCB116-d5 at 100 µg·mL⁻¹ in iso-octane were purchased from Cluzeau Info Lab[®] (France).

140

141 **2.4 PCB extraction and analysis**

142 Prior to extraction, sediments were dried with anhydrous sodium sulfate and ground into fine powder. PCB 116-d5 was spiked before the extraction of all samples and used as an internal 143 standard. Sediments, glass fiber filters, PUF plugs and PUF disks were extracted by an Accelerated 144 145 Solvent Extractor (ASE 200 Dionex®) at 100°C and a pressure of 138 bar for 3 cycles with a mixture of (50:50 v/v). C18 filters were 146 acetone/dichloromethane eluted with 10 mL of 147 heptane/dichloromethane (80:20 v/v) followed by 10 mL of heptane/dichloromethane (98:2 v/v). The extraction and clean-up of fish samples are described elsewhere²⁷. 148

149 Prior to cleanup, only the sediment samples were treated with an acid-activated copper powder to 150 remove sulfur. Then, all extracts were concentrated to 2 mL using a TurboVap® II and purified on an SPE column loaded with 3 g of silica, eluted successively with 15 mL of a mixture of 151 heptane/dichloromethane (98:2 v/v) and 10 mL of heptane/dichloromethane (80:20 v/v). Eluates 152 153 were reconcentrated to 1 mL and passed through a 0.2 µm PTFE filter. They were evaporated near 154 dryness with nitrogen and resuspended in 100 µL of heptane for analysis. All PCB solutions were 155 analyzed using a Clarus 580 gas chromatograph from Perkin-Elmer® with an Optima® HP-5-MS accent 156 30 m x 0.25 mm nonpolar fused silica capillary column from Macherey-Nagel® coupled with a pulsed discharge detector in photoionization mode (Vici®). The samples were injected in splitless mode at 157 158 300°C. Helium was used as the carrier gas (1.0 mL·min⁻¹). After injection, the oven temperature was set to 60°C for 1 min and increased gradually at a rate of 10°C/min to 240°C and then at a rate of 159 160 5°C/min to 320°C, and then remained steady for 5 min.

161 **2.5 Quality control**

Quantification was ensured for the 7 indicator PCB congeners (PCBi = PCB28, 52, 101, 118, 153, 138, 162 180) as they represent approximately 50% of the compounds found in Pyralene[®] mixtures²⁸. 163 Calibration curves were established with authentic standards (Fig. S2). Extraction yields were 164 165 determined from certified material (sediment) or from spiked material (water, air samples) (Tab. S1). 166 Extraction yields were not used for correction, and normalization to PCB116-d5 values spiked before extraction accounted for extraction correction. Detection limits were determined as the mean 167 168 response plus three times the standard deviation of procedural blanks for each PCB (Tab. S2). When 169 appropriate, field blanks were subtracted from the sample concentrations to avoid false positives. 170 Unless specified, every PCB concentration, flux and mass budget mentioned hereafter refer to 171 Σ7PCB_i.

172 **2.6 Calculation**

173 Air/water gaseous PCB exchange model:

174 The net gas exchange of PCBs across the air–water interface, F_{aw} (mol·m⁻²·s⁻¹), is given by equation 175 (1):

176

$$F_{aw} = K_{ol} \left(\frac{C_a}{H'} - C_w \right) \tag{1}$$

where K_{al} is the overall mass transfer coefficient (m·s⁻¹), H' is the temperature-corrected Henry's law 178 coefficient (dimensionless), and C_a and C_w are the dissolved PCB concentrations (mol·m⁻³) in air and 179 180 water, respectively. A positive F_{aw} represented a net input of PCBs from the air into water, and a 181 negative F_{aw} represents a net volatilization of PCBs. The Henry's law coefficient values (H) presented 182 in the literature can vary by two orders of magnitude. In this study, H values were collected from the compilation of Sander et al.²⁹. The minimum and maximum values were disregarded and mean ± 183 standard deviation values were obtained (Tab. S3) and used for air/water exchange calculations and 184 propagation analysis. 185

More details regarding input parameter calculations for air/water exchange modeling (i.e., *K_{ol}*, H', C_a
 and C_w) are described in the Supporting Information.

188 Settling particle flow:

- 189 The settling particle flow F_{sed} (g·yr⁻¹) was calculated as follows in equation (2):
- 190

$$F_{sed} = C_{sp} \operatorname{Rsed}_{85m} A_b \tag{2}$$

(3)

where F_{sed} is the PCB settling rate (g·yr⁻¹), C_{sp} is the mean PCB concentration of the settling particles (g·kg⁻¹), $Rsed_{85m}$ is the settling rate at the lake mean depth (85 m) (kg·m⁻²·yr⁻¹), and A_b is the surficial sediment surface of lake Bourget (m²).

194 $Rsed_{85m}$ was calculated using equation (3) as recently proposed by Corcoran et al.³⁰, suggesting that 195 settling rates are related to depth, following a power-law relationship:

196
$$Rsed_x = 1.91x^{-0.90}$$

197 $Rsed_{40m}$ calculated with equation (3) (i.e., 0.07 g·cm⁻²·yr⁻¹) was half of $Rsed_{40m}$ experimentally 198 determined from the sediment trap (i.e., 0.14 g·cm⁻²·yr⁻¹). This could be explained by (i) a much larger 199 catchment area/lake surface area ratio in Lake Bourget (i.e., 13) compared to that of the American 200 Great Lakes³⁰ (i.e., 1.8 – 3.37), which could result in higher suspended material loads to the lake³⁰ and 201 (ii) a higher primary production rate enhanced by the important precipitation of calcium carbonate in 202 summer³¹. Therefore, $Rsed_{85m}$ estimated from equation (3) was multiplied by a factor of 2 to offset 203 this gap.

204 Tributary flows

The inflow of PCBs into Lake Bourget were due to three main sources, identified as the Leysse River,the Tillet River and Terre-Nue Canal.

PCBs entering the lake through the three tributaries could be estimated individually as follows in equation (4):

$$Fin_{Trib} = Cw_{Trib} * Qm_{Trib} * 365$$
(4)

209

- 210 where Fin_{Trib} is the annual PCB input through the tributary, Cw_{Trib} is the total PCB concentration in
- the water at the tributary output (ng·L⁻¹), Qm_{Trib} is the water flow (L·d⁻¹) and t_{Trib} is the time of the experiment (d).
- For the Tillet River, the fluxes were determined considering two distinct meteorological situations (i.e., dry and rainy weather), as inputs could be impacted by a change of flow and a change of water PCB concentration due to the remobilization of contaminated particles from the riverbed sediment.
- 216 Atmospheric deposition
- PCB input by deposition onto the lake surface (F_{ad} in ng·yr⁻¹) was calculated as follows in equation (5):
- 219

 $F_{ad} = F_a A_l \tag{5}$

where F_a is the measured bulk deposition mean flux (ng·m⁻²·yr⁻¹) deduced from the PUF collected in the Owen Gauge and A_l is the Lake surface area (m²).

222 Outflow

The Savières Canal was identified as the sole outlet for Lake Bourget water. PCB annually outflowing the lake through the Savières Canal, F_{out} (g·yr⁻¹), could be estimated using equation (6):

225
$$F_{out} = C_w * Q_m * 365$$

where C_w is the mean total (dissolved + particulate) PCB concentration of the lake water (ng·L⁻¹), Q_m is the mean river flow (L·d⁻¹) and t (d) is the time of the experiment.

(6)

228 Output through fishing activity

The quantity of PCBs withdrawn from the lake via fishing (F_{fish} in g.yr⁻¹) was estimated with equation (7):

$$F_{fish} = C_{fish} m_{fish}$$
(7)

where C_{fish} is the concentration in the fish filets (ng·gW·W⁻¹) and m_{fish} is the mass of fish captured each year (g·yr⁻¹).

234

235 Sediment-water diffusion flux

236 Sediment-water diffusion flux, F_{sw} (g·yr⁻¹), was calculated using equation (8):

237
$$F_{sw} = [-V_{diff} (C_w - C_{wp})] A_b$$
(8)

where A_b is the surficial sediment surface (m²), C_w is the lake water-dissolved PCB concentration (g·m⁻³), C_{wp} is the pore water PCB dissolved concentration (g·m⁻³), and V_{diff} is the estimated sediment-water exchange velocity (m·yr⁻¹). A positive F_{sw} value corresponds to a net flux of PCBs from the sediment to the water column. The sediment surface A_b was divided into five zones (zones I – V) of the same surface around the five sediment sampling locations along the north-south transect to account for heterogeneous sediment contamination (Fig. S3). More information about the calculation of V_{diff} and C_{wp} can be found in the SI.

245 *Resuspension:*

246 The resuspension of PCBs from the surficial sediment, $F_{res}(g\cdot yr^{-1})$, was calculated with equation (9):

 $F_{res} = C_s R_{res} A_b \tag{9}$

where C_s is the surficial sediment PCB concentration (g·g_{DW}⁻¹), A_b is the lake sediment surface, and R_{res} (547 g·m²·yr⁻¹) is the resuspension rate estimated by Eadie et al.³² for lake Michigan. This value was used to calculate of F_{res} since the main parameters affecting resuspension rates (i.e., water column depth, wind speed, bioturbation) were relatively similar for both Lake Michigan and Lake Bourget.

253 Sediment Burial flow:

The sediment burial flow represents the quantity of PCBs being buried and no longer accessible for resuspension or bioturbation, as they are supposed to be permanently removed from the water column³³.

257 The sediment burial flow was calculated with equation (10):

 $F_{sed} = C_s A_{acc} R_{sed(acc)}$ (10)

where C_s is the mean sediment PCB concentration (g·kg_{DW}⁻¹), A_{acc} is the surface of the bottom of the lake that allows sediment accumulation, calculated as described by Blais et al.³⁴ The A_{acc} for lake Bourget was estimated to be 11 km².

262 $R_{sed(Aacc)}$ ' is the converted accumulation rate (kg·m⁻²·yr⁻¹) calculated with equation (11):

263

$$R_{sed(Aacc)}' = R_{sed(Aacc)} \rho_{sed} \tag{11}$$

where $R_{sed(Aacc)}$ is the accumulation rate (m³·m⁻²·yr⁻¹) previously measured at the deepest point of Lake Bourget²⁵ and ρ_{sed} is the sediment density (kg·m³).

266 Net PCB mass balance:

The net PCB mass balance, F_{net} (g·yr⁻¹), was calculated with equation (12) by subtracting the outputs from the inputs without accounting for internal processes:

269 $F_{net} = F_{trib} + F_{ad} - (F_{aw} + F_{sed} + F_{fish} + F_{out})$ (12)

A positive F_{net} means that the lake is accumulating PCBs, whereas a negative F_{net} shows a decrease in PCB contamination.

272 An appropriate conversion factor was applied to all fluxes to express the results in $(g\Sigma 7PCB_i \cdot yr^{-1})$ to 273 facilitate intercomparison.

- 274 Water inventory
- 275 The total mass of the PCBs in water I_{water} (g) was calculated as follows using equation (13):
- $I_{water} = C_w V_w \tag{13}$
- where C_w is the total (dissolved + particulate) PCB concentration in the lake water (g·m⁻³) and V_w is the volume of the lake water (3.6 × 10⁹ m³).
- 279 Sediment inventory
- The total mass of the PCBs in the surficial sediment, $I_{sediment}$ (kg) (0 4 cm), was estimated with equation (14):

282
$$I_{sediment} = \sum_{i=1}^{V} 4(Cs_i \rho s_i)$$
(14)

where Cs_i is the PCB concentration in the sediment in the first centimeter of the five cores corresponding to zones I to V (kg·g⁻¹) and ρs_i is the sediment density in zones I to V (g·cm⁻³). A factor of 4 is applied to expend the stock in the first centimeter of sediment to the 4 cm of the surficial sediment.

287 *Residence time of PCBs*

The residence times in the water (τ_{water}) and in sediment (τ_{sed}) (in days) were calculated as follow in order to be consistent with the methodology applied for the Lake Michigan Mass Balance Project¹:

290
$$\tau_{water} = \frac{I_{water}}{F_{aw} + F_{out} + F_{set} + F_{sw}}$$

291 and

292
$$\tau_{sed} = \frac{I_{sediment}}{F_{sed} + F_{res}}$$

293

294 **2.7 Error propagation analysis:**

295 To estimate the impact of the uncertainty of the input parameters on the PCB fluxes, error 296 propagation analysis was performed considering uncertainties in the input parameters (Cw, Ca, H, Kol, 297 fom and C_s). Uncertainties in C_s, C_w and C_a were linked to year-to-year variability, measurement errors 298 and random analysis errors (see Tab. 1), whereas the uncertainties in H, K_{ow} and the diffusive 299 boundary layer thickness (δbl) values were discussed above and mentioned in Tab. S3. An 300 uncertainty of 40% for K_{ol} (including the uncertainty in wind speed and water (K_w) and air (K_a) mass 301 transfer coefficient estimates) was assumed as commonly accepted ^{9,35–37}. Error propagation analysis with 302 R software using the package "propagate" was performed (https://cran.rproject.org/web/packages/propagate/propagate.pdf). The software calculated the error propagation 303 304 using first-order Taylor expansion accounting for a full covariance structure using a matrix-based 305 approach.

306

307 3. <u>Results and discussion</u>

308 3.1 Inputs

309 Tributaries

SPM-bound PCBs entering the lake for both the dry and rainy periods were estimated at $23 \pm 3 \text{ mg} \cdot d^{-1}$ and $146 \pm 85 \text{ mg} \cdot d^{-1}$, respectively. A nonnegligible part of the PCB input could be attributed to freely dissolved PCBs with fluxes of $15 \pm 2 \text{ mg} \cdot d^{-1}$ and $61 \pm 8 \text{ mg} \cdot d^{-1}$ in the dry and rainy periods, respectively. Therefore, the total input into the lake (SPM-bind + dissolved PCBs) was estimated at 21 $\pm 6 \text{ g} \cdot \text{yr}^{-1}$. Larger fluxes recorded for the rainy period were due to (i) riverbank erosion, (ii) a higher water flow due to precipitation and (iii) a substantial resuspension of the highly contaminated riverbed sediment.

The annual flow of the Terre-nue canal over the 2014-2015 period was 0.15 $m^3 \cdot s^{-1}$ (CISALB, personal communication). The PCB (dissolved + particulate) concentrations in the river water were 6.5 $ng \cdot L^{-1}$

and 4.3 ng·L⁻¹ in 2014 and 2015, respectively ("Agence de l'eau RMC"). Therefore, the PCB fluxes
 entering the lake through Terre-nue canal could be estimated at 24 ± 5 g·yr⁻¹.

The PCB (dissolved + particulate) concentrations were measured in the Leysse River by the "Agence 321 de l'eau RMC" in water from 2011 to 2014 (n = 27)²⁴. Unfortunately, water PCB concentration data 322 were not available for the period 2015-2017. PCB concentrations for 2015-2017 were estimated from 323 324 the mean value of the data from 2011 to 2014 since a steady contamination was observed for this 325 period. Nondetectable values in the "Agence de l'eau RMC" dataset were substituted by LQ/2, as generally accepted³⁸, and were suitable for basic data processing³⁹. Therefore, the mean PCB 326 327 concentration was estimated at 3.5 ± 0.5 ng·L⁻¹ and was mainly represented by high-molecular-328 weight PCBs. The mean water flow (2015-2016) of the Leysse River was 6.5 m³·s⁻¹ (CISALB, personal communication). Hence, the annual flux of PCBs entering the lake through the Leysse River was 329 330 estimated at 724 \pm 100 g·yr⁻¹.

PCB annual inflows through the three main tributaries can be estimated at 769 \pm 100 g·yr⁻¹. The major contributor to PCB inflow in the lake was identified as the Leysse River, mainly because of a higher water flow since the PCB water concentration was on the same order as in the Tillet River and Terro Nuc Canal

- 334 Terre-Nue Canal.
- 335

336 Atmospheric deposition

Eighteen samples were analyzed and showed a mean deposition flux of 1.4 ± 0.7 ng·m⁻²·d⁻¹. A 337 338 seasonal variation was observed, with higher fluxes recorded in the winter than in the summer (i.e., 339 1.6 \pm 0.8 ng·m⁻²·d⁻¹ and 1.0 \pm 0.5 ng·m⁻²·d⁻¹, respectively). The PCB profile was dominated by PCB153 340 (27%) but was evenly distributed between low- and high-molecular weight congeners. An increase in 341 the contributions of PCB101, 153, and 138 was observed in the winter compared to the summer. A 342 possible explanation is that heavy PCBs represent a lower proportion of the total gaseous PCBs in the 343 summer (data not shown). Consequently, the heavy PCBs are less exposed to dry and/or wet 344 deposition during this period. Altogether, the average PCB input to the lake through atmospheric deposition for the period 2013-2016 was $23 \pm 12 \text{ g·yr}^{-1}$. 345

346 Uncertainties related to the inputs from rivers and the atmosphere were rather restricted. Indeed, 347 every parameter necessary for the flux calculation was measured, and the need for modeling or 348 extrapolating data was limited. However, uncertainty regarding the inputs through the Leysse River remains nonnegligible. The quantification limits communicated by "Agence de l'eau RMC" for 349 350 individual PCBs were elevated (i.e., from 0.3 to 1.2 $ng L^{-1}$). Therefore, the substantial number of 351 nondetectable values (replaced by LQ/2 in the calculations) in the dataset could have led to an 352 overestimation of the PCB concentration, and consequently, to an overestimation of PCB inputs. 353 However, the sediment concentration of the Leysse river sediments recorded by "Agence de l'eau RMC" (5 – 33.5 $ng \cdot gD \cdot W^{-1}$) for the period 2013 to 2017 and the concentration measured in the Leysse 354 River plume zone in Lake Bourget (75 ng·gD·W⁻¹) in 2005⁴⁰ are important. These results support the 355 high levels of PCB contamination recorded in the water and strengthen our hypothesis that the 356 357 Leysse River is currently the major source of PCBs in Lake Bourget.

358 3.2 Internal flows

359 Settling

Samples representing an integrative settling particle flux for a full year (July 2016 to June 2017) could
 be retrieved from the automatic sediment trap and analyzed. The total sediment dry weight

362 collected was 1400 g, and the settling rate was 0.14 g·cm⁻²·yr⁻¹. The mean PCB concentration in the 363 settling particles from the three sediment traps across the lake (n = 5) was 56 ± 39 ng·g_{DW}⁻¹ and was 364 assumed to be representative of the whole lake. The PCB congener profile was mainly composed of 365 heavy PCBs (PCB 153, 138, 180 > 75% Σ 7PCB_i). Hence, the annual flux of PCBs to the sediment 366 through settling was estimated at 1721 ± 1214 g·yr⁻¹.

367 Resuspension

The resuspension of PCBs from the sediment was calculated for zones I – V to account for discrepancies in sediment PCB concentration at the five sampling locations (Tab. 1). Resuspension from the sediment concerned mostly PCBs with a high affinity for organic matter (i.e., PCB153, 138, 180 > 75%). By adding the results for zones I – V, an annual resuspension flux of 1648 ± 549 g·yr⁻¹ was deduced.

373 Diffusive water/sediment PCB exchange flux

374 Diffusive water/sediment PCB exchange flux was estimated for zones I to V. Every PCB congener 375 showed sorption to surficial sediment in every zone except for PCB28, which diffused from the 376 sediment to the water in zones II, IV and V. Generally, the PCB flux profile was relatively similar between sites and was dominated by PCB101 (20%) and PCB138 (25%) (Fig. S4 in SI). The sorption 377 rates of PCBs were similar in zones I, II, III and V, with a flux of 3.25 – 4 µg·m²·yr⁻¹. However, a lower 378 379 flux was calculated for zone IV (1.7 $\mu g \cdot m^2 \cdot yr^{-1}$). This was due to the higher PCB concentration in the 380 sediment of zone IV compared to the other zones. Overall, the sorption flux from water to sediment 381 was estimated at 143 \pm 62 g·yr⁻¹.

382 Error propagation analysis was performed and included a measurement in the uncertainty of Cw, Cs, 383 f_{OM} , K_{ow} and δbl . An uncertainty of 76–100% was associated with the flux of PCBs in every zone 384 except zone IV (191%). The relative contribution of input parameter uncertainty to the sorption flux 385 uncertainty was investigated. The flux uncertainty was mainly associated with C_w (45%), δbl (16%) 386 and K_{ow} (14%). In the case of the diffusion from sediment to water, the flux uncertainty was related 387 to C_s (41%), K_{ow} (26%), C_w (15%) and δbl (14%). Thus, it is critical to correctly assess C_s and C_w to perform the modeling of this flux, but a wise choice of δbl and K_{ow} values also enhances the accuracy 388 389 of the model.

390 Overall, the internal flux $(F_{set} + F_{sw} - F_{res})$ was 70 ± 1334 g·yr⁻¹. Therefore, this system could be 391 considered at equilibrium and was not included in the net PCB mass budget hereafter.

392 3.3 Outputs

393 Air/water gaseous PCB exchange

The model showed a mean net PCB volatilization of 54 ng·m²·d⁻¹ from the surface of Lake Bourget. 394 395 Every PCB congener outgassed, and the volatilization profile was evenly represented by low- and 396 high-molecular weight PCBs (i.e., mainly PCB28, 52 and 153, Fig. S5 in SI). A seasonal pattern was 397 observed since monthly fluxes of PCB volatilization were on average 35% higher in the period of May to August than in the rest of the year. However, the PCB volatilization profile remained fairly 398 399 constant throughout the year. The higher fluxes observed in the summer were due to (i) a warmer 400 lake water temperature and (ii) a lower gaseous PCB concentration (i.e., mean Σ 7PCB_i (summer) = 401 35.0 pg·m⁻³ and mean Σ 7PCB_i (winter) = 127.3 pg·m⁻³).

402 The influence of the input parameters can vary depending on the direction of the flux (i.e., 403 volatilization or absorption), as recently demonstrated by Liu et al.⁹ Therefore, measurement errors 404 regarding the input parameters or an unwise choice in H values for computing could critically affect 405 the flux calculation because it could lead to great uncertainties in the resulting flux. According to Liu 406 et al.⁹, when volatilization dominated, the main input parameters influencing the flux were C_w and 407 K_{ol} .

408 To identify the relative contribution and the effects of the uncertainty from the input parameters to 409 the flux uncertainty, an error propagation analysis was performed for individual PCB congeners. 410 Overall, an uncertainty of 55% was computed for the yearly flux of PCB. This output was similar for 411 Lake Ontario and Lake Erie⁹. The relative contribution of parameter uncertainty to the flux 412 uncertainty was mainly related to C_w (86%) and K_{ol} (13%). This result was consistent with the control 413 of C_w and K_{ol} over the flux intensity in the case of volatilization⁹. Nonetheless, the importance in the 414 choice of H value for modeling should not be minimized. Indeed, flux modeling with the minimum 415 and maximum individual PCB H values (among those retained for this study (n = 10) from the Henry's law compilation from Sander²⁹) led to a variation of 209% in the PCB volatilization flux when every 416 417 other input parameter was fixed. Altogether, the volatilization flux of PCBs was 861 ± 473 g·yr⁻¹.

418 Sediment burial

The sediment burial flow was calculated for the accumulation zone of Lake Bourget (i.e., 11 km²). The

PCB congener profile of the buried sediment was mainly composed of heavy PCBs (PCB153, 138, 180
 > 80%, Fig. S6), as could be expected from the high affinity of these highly chlorinated molecules for

422 organic particles. An annual flux definitively incorporating the anoxic sediment of $3408 \pm 2404 \text{ g·yr}^{-1}$

423 was estimated. This elevated flux was mainly due to the intensity of the accumulation rate as a result

- 424 of a high settling rate combined with an important resuspension of SPM-bound particles eventually
- 425 accumulated at the bottom of the lake.
- 426 Outflow

427 Outflow was only possible through the Savières Canal. The mean water flow was 13.4 m³·s⁻¹, and the 428 total lake water concentration was 518 \pm 96 pg·L⁻¹. Therefore, the average annual flow of PCBs

429 exiting the lake was estimated to be $220 \pm 41 \text{ g·yr}^{-1}$.

430 Output through fishing activity

The mean PCB concentration in fish filets for the period 2013-2017 was $258 \pm 90 \text{ ng} \cdot \text{gW} \cdot \text{W}^{-1}$ and $47 \pm 26 \text{ ng} \cdot \text{gW} \cdot \text{W}^{-1}$ for arctic char and whitefish, respectively. The average annual capture (professional and recreational) of arctic char and whitefish was 4 and 95 tons, respectively, for the period 2014-2017 (S. Cachera, personal communication). Therefore, the annual output through fishing activity was $5 \pm 1 \text{ g} \cdot \text{yr}^{-1}$.

436 **<u>3.4 PCB inventory in Lake Bourget</u>**

The net flow of PCBs in Lake Bourget exiting the lake water column for the period 2013-2017 was 3701 \pm 2452 g·yr⁻¹ and was mainly due to sediment burial and volatilization (Fig. 1). This net output was consistent with a diminution of the lake contamination, as suggested by the decreasing PCB contamination observed in the biota since 2008²⁷.

The stock of PCBs in the lake water column was estimated from the water total PCB concentration and the volume of the lake. A stock of 1865 ± 353 g of PCBs was estimated to remain in the water column, both in dissolved and particulate form, potentially susceptible to bioaccumulation in the biota. This stock is expected to decline due to the negative net flow of PCBs in Lake Bourget. The residence time of PCBs in the water column was estimated at 231 ± 72 days. This results is similar to

that of Guo et al. (2017)⁴¹ in Lake Michigan and highlights the relatively rapid dynamics of PCBs in 446 447 water. A stock of PCBs in the lake surficial sediment (0-4 cm) for zones I to V of 181 ± 60 kg was 448 estimated. This represents the quantity of PCBs potentially available for resuspension, bioturbation 449 or diffusion to the water column. Moreover, the residence time of PCBs in the surficial sediment was 450 estimated at 36 ± 20 years. Therefore, the high quantity of PCBs in the sediment associated with a 451 long residence time cannot be neglected and raises concern even though this stock is expected to 452 become progressively lower with the progressive deposition of cleaner sediment due to the 453 continuous decrease in the PCB concentration in the water column.

In this work, photo-degradation of PCBs in the euphotic zone as well as biodegradation processes in
 the anoxic compartment of the sediment were considered negligible. Therefore, the impact of these
 processes in the removal of PCBs from these two compartments were neglected.

457

458 **3.5 Main fluxes driving PCB decontamination in Lake Bourget**

459 Importance of PCB loads from tributaries to perialpine lake contamination

460 The input of PCBs into Lake Bourget was mainly due to inflow from contaminated tributaries rather 461 than from atmospheric inputs (i.e., dry and wet deposition + gaseous absorption). This is in contrast with other lakes, such as lake Michigan and Lake Superior, where atmospheric inputs contribute 462 more than tributaries^{2,3}. Two possible explanations are (i) the catchment area over the lake surface 463 area ratio was 13 for Lake Bourget and 0.6–1.5 for the American Great Lakes, which enabled a larger 464 465 contribution from atmospheric deposition in the latter and (ii) the much higher water residence time (i.e., 99 years in Lake Michigan and 8 years for Lake Bourget) could justify the lower PCB input 466 467 through tributaries. However, our results were consistent with those of Gevao et al.⁴ for a small rural 468 lake (Lake Cumbria) in the UK with a high catchment area to lake surface area ratio (i.e., 17). As 469 expected, the contribution of the Tillet River was very low (21 g·yr⁻¹) and diminished drastically 470 compared to the prior sediment clean-up (1500 g·yr⁻¹). Consequently, the Leysse River should 471 currently be considered as the main source of PCBs in Lake Bourget.

Altogether, our results suggest that as in the American Great Lakes^{2,3}, losses through sediment burial and volatilization largely overcame any other fluxes. This observation was rather consistent with previous studies reporting the PCB mass budget of several American Great Lakes exhibiting high levels of PCBs in the water column. However, some discrepancies about the relative contributions of these fluxes to the PCB net losses were noted.

477 Sediment burial as a driver for the loss of PCBs

The sediment burial contribution was larger in Lake Bourget (i.e., 76%) than in the American Great 478 479 Lakes (i.e., 27%²). This observation was mainly related to dissimilarities in the accumulation rates 480 rather than in the PCB contamination of surficial sediment. The high accumulation rate recorded in Lake Bourget could be related to the fact that despite a constant decrease since the peak 481 482 eutrophication in the 1970s, Lake Bourget primary production remains higher than in the American Great Lakes (Chlorophyll α concentration = 3.3 mg·m⁻³ vs 0.75 mg·m⁻³, respectively⁴² and total 483 phosphorus = 9 μ g·L⁻¹ vs 7 μ g·L⁻¹ respectively^{16,43}). Therefore, the effect of the biological pump 484 485 coupled with a high settling flux that drives organic contaminants from the euphotic zone to the sediment could partly explain the intensity of the sediment burial flux of PCBs. In addition, the 486 important SPM loads from the tributaries contributed in part to the high accumulation rate. 487 488 Furthermore, the binding of the more hydrophobic PCBs to the suspended particles should directly impact the intensity of the sediment burial of PCBs and its contribution to lake decontamination. If the efforts towards reoligotrophication remains effective in the future, primary production and PCB sediment burial flux should continue to decline. However, in the context of climate change, an increase in the water temperature could enhance the primary production and counterbalance or overcome the former effect.

494 Impact of volatilization in the lacustrine decontamination process: observations and 495 perspectives

The estimated net volatilization rate of 54 \pm 30 ng·m⁻²·d⁻¹ was high compared to Lake Erie and Lake 496 Ontario (2.9 and 9 ng·m⁻²·d⁻¹, respectively)⁴⁴ but was on the same order as that of Lake Michigan (52 \pm 497 498 22 $ng \cdot m^{-2} \cdot d^{-1}$)² and Lake Cumbria⁴ (192 $ng \cdot m^{-2} \cdot d^{-1}$). This net volatilization is closely related to the 499 dissimilarities in PCB water concentration because it is the main parameter driving the flux intensity 500 in the case of volatilization, as stated earlier. Indeed, the water concentrations were low in Lake Erie 501 and Lake Ontario (33.9 and 29.1 pg·L⁻¹, respectively)⁴⁴ compared to Lake Michigan (190-300 pg·L⁻¹)² and Lake Cumbria (2000 pg·L⁻¹)⁴⁵. Considering that the surface area/volume ratio of Lake Bourget is 502 503 comparable to Lake Michigan (12.8 and 11.8, respectively) and that the volatilization rate is of the 504 same order, volatilization contributes similarly to the PCB decontamination of the water column in 505 both lakes. The higher average water surface temperature in Lake Bourget compared to Lake 506 Michigan (i.e., 15.5°C and 10°C, respectively^{16,46}) did not significantly impact the magnitude of the 507 volatilization process or its relative contribution to the loss of PCBs from the lake. Even though it was 508 not investigated in this study, a seasonal variability of the volatilization process is expected to occur. 509 Indeed, volatilization has been shown to be related to processes that are season-dependent such as temperature⁴⁷, thermal stratification^{48,49} or plankton abundance^{50,51}. 510

511 An important rise in the water temperature is expected in the near future. These trends will be 512 magnified in small- to medium-sized water bodies, such as perialpine lakes, which are more sensitive 513 to variations in the air temperature than large lakes. An increase in surface water temperature will 514 impact the biogeochemical processes of PCBs. Among the perturbation of other mechanisms such as 515 partitioning to particulate matter or enhanced uptake by the biota such as described in the work of 516 Meijer et al.⁵², an increase of temperature could also thermodynamically favor the volatilization of 517 PCBs. Therefore, it could ultimately enhance the relative contribution of this flux to the overall PCB 518 mass budget.

This PCB mass budget revealed important discrepancies compared to previously investigated ecosystems (i.e., the American Great Lakes and high-altitude lakes) and brings new insights into the processes ruling PCB dynamics in perialpine lakes. Most of the perialpine lakes in Europe present similar characteristics (i.e., high catchment basin/lake surface area ratio, similar surface area/volume ratio, low water residence time, highly urbanized and industrialized watershed) to Lake Bourget. Therefore, the PCB mass budget investigated in this work should be applicable to similar lakes across the world (e.g., Lake Geneva, Lake Maggiore).

526 Impact of uncertainties in the estimation of PCB fluxes

The contribution of uncertainties in the PCB concentration of environmental samples to the modeled flux uncertainties highlighted the importance of an accurate determination of PCB concentration in every studied matrix. As an example, PCB concentration in sediment must be precisely measured for the calculation of diffusion at the water/sediment interface and sediment burial fluxes. Similarly, measurements of the truly dissolved PCB concentration for air/water exchange modeling are also recommended since only truly dissolved PCBs are available for volatilization. This measurement 533 remains challenging, and it has been shown that ~35% of PCBs were not retained by conventional filtration of particles due to binding to colloids⁵³. Colloid-bound PCBs included in the dissolved PCB 534 535 fraction would lead to an overestimation of the dissolved PCB concentration and volatilization flux. Therefore, the determination of the water-dissolved PCB concentration using passive sampling 536 techniques is recommended and leads to robust results^{44,54}. These cheap and easily operated 537 538 techniques should encourage the performance of triplicate measurements to reduce measurement 539 uncertainties. Moreover, these techniques allow time-weighted average concentration measurements and could be used to obtain mean water concentration with a moderate temporal 540 541 resolution within a timeframe of a few weeks. The error propagation analysis also highlighted the 542 importance of the wise choice of constants for the accurate estimation of modeled fluxes. 543 Consequently, a careful, exhaustive review of the literature available should be performed before assigning H and Kow values to the flux calculation. Relying on at least a review paper rather than on 544 545 only one source is highly recommended. When possible and appropriate, field measurements should 546 be performed to lessen the use of inconsistent constant values or partition coefficients in flux 547 modeling.

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Compartment	n	Monitoring period	Mean ± sd
Water, tributary (ng.L ⁻¹)			
Terre-Nue canal	2	2014-2015	5.3 ± 1.0
Leysse River	4	2010-2014	3.5 ± 0.5
Tillet River (dissolved fraction only)	3	2017	1.8 ± 0.2
Water, Lake (dissolved) (pg.L ⁻¹)	5	2015-2016	384 ± 170
Water, Lake (total) (pg.L ⁻¹)	3	2015-2016	518 ± 96
Air, gas (pg.m ⁻³)	9	2014-2016	47 ± 18 (summer) 106 ± 70 (winter)
Sediment core, Lake (0 – 1cm) (ng.g _{DW} -1)			
Zone I	2	2013-2015	47 ± 43
Zone II	1	2015	52
Zone III	2	2013-2015	59 ± 64
Zone IV	3	2013-2016	121 ± 15
Zone V	3	2013-2016	61 ± 82
Fish filet (ng.g w.w ⁻¹)	248	2013-2017	258 ± 90 (arctic char) 47 ± 26 (whitefish)
Water Temperature (°C)	24	2015-2016	18 ± 4 (summer) 8.1± 2.3 (winter)
Wind speed (m.s ⁻¹)	24	2015-2016	2.1 ± 0.3 (summer) 2.4 ± 0.4 (winter)

Table 1: Σ7PCB_i concentrations in the Lake Bourget ecosystem and meteorological parameters used for model computation (n = number of samples, sd = standard deviation).



Fig. 1: PCB mass budget (mean ± sd) of Lake Bourget (2013-2017). The green area represents the surficial sediment of the lake.

